

INDUSTRY GUIDE

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# Steel Ladle Refractory Solutions: Working Lining, Safety Lining, and Castable Systems

Complete guide to multi-layer ladle lining design, material selection for 50-200 heat campaigns, and bottom impact pad optimization.

Steel ladle refractory lining systems employ a multi-layer configuration to balance thermal protection, structural integrity, and campaign life for 50-200 heat cycles. The standard three-layer design consists of: (1) a **working lining** in direct contact with the molten metal, typically constructed from magnesia-alumina spinel brick ( $\text{MgO} \cdot \text{Al}_2\text{O}_3$ ), magnesia-carbon brick ( $\text{MgO} \cdot \text{C}$ ), or ultra-high alumina (UHA) brick; (2) a **safety lining** (permanent layer) providing thermal backup and structural support, commonly using high alumina brick; and (3) a **bottom impact pad** — a wear-resistant castable zone absorbing the kinetic energy and thermal shock during tapping.

Material selection follows ASTM C401 for monolithic refractories and GB/T 2992 for magnesia-alumina refractories, including refractoriness under load (RUL)  $>1600^\circ\text{C}$ , slag penetration resistance, thermal shock stability, and resistance to argon stirring systems. Industry data from continuous casting operations indicates working lining campaigns of 50-100 heats for ultra-high alumina spinel brick, 100-200 heats for magnesia-carbon brick (with proper slag chemistry control), and 150-250 heats for high alumina brick. Total cost of ownership must account for material cost, installation labor, ladle turnaround time, and the cost of downtime during working lining campaigns).

## Steel Ladle Structural Configuration and Thermal Zones

A typical steel ladle lining consists of distinct functional layers, each serving specific thermal, mechanical, and chemical functions. The working lining is the innermost layer, directly exposed to the molten metal. The safety lining provides thermal backup and structural support. The bottom impact pad is a wear-resistant castable zone designed to absorb the kinetic energy and thermal shock during tapping.

| LAYER             | FUNCTION                                             | TYPICAL MATERIAL                                            |
|-------------------|------------------------------------------------------|-------------------------------------------------------------|
| Working Lining    | Direct steel & slag contact, primary thermal barrier | Magnesia-alumina spinel brick / MgO-C bric ULCC             |
| Safety Lining     | Thermal backup, structural protection                | High alumina brick (75–85% Al <sub>2</sub> O <sub>3</sub> ) |
| Bottom Impact Pad | Absorb tapping impact & thermal shock                | ULCC with SiC or corundum aggregates                        |
| Steel Shell       | Structural containment                               | Carbon steel (6–25mm plate)                                 |

**Key Design Principle:** The working lining is a consumable component designed for periodic replacement, w structural backup. Proper installation of the safety lining extends total ladle service life and reduces downtir without full ladle rebuilds.

## Working Lining Material Selection and Performance Comparison

Working lining material choice depends on steel grade, tapping temperature, slag basicity, argon stirring i material families each offer distinct performance characteristics:

### Magnesia-Alumina Spinel Brick (MA Spinel)

Magnesia-alumina spinel brick combines MgO and Al<sub>2</sub>O<sub>3</sub> to form a synthetic spinel phase (MgO·Al<sub>2</sub>O<sub>3</sub>), off stability. Typical composition: MgO 60–75%, Al<sub>2</sub>O<sub>3</sub> 15–30%, with bulk density 2.9–3.1 g/cm<sup>3</sup> and cold crus

#### Advantages:

- Superior resistance to both acidic and basic slags due to amphoteric nature of spinel
- Good thermal shock resistance (better than MgO-C in rapid cycling operations)
- Lower thermal conductivity than MgO-C (reduces shell temperature)
- No carbon oxidation concerns (unlike MgO-C brick)

**Typical Campaign Life:** 80–150 heats in continuous casting ladles

**Best Applications:** Ladles with high slag volumes, argon stirring, or frequent thermal cycling

### Magnesia-Carbon Brick (MgO-C)

Magnesia-carbon brick incorporates graphite (8–20% C) into a magnesia matrix, providing exceptional slag resistance behavior. Typical composition: MgO 75–85%, C 10–18%, with antioxidants (Al, Si powder).

#### Advantages:

- Highest slag resistance — graphite phase prevents slag infiltration
- Excellent thermal conductivity (rapid heat dissipation, lower hot face temperature)
- Good erosion resistance under argon stirring
- Longest campaign life potential (100–200 heats with optimized slag chemistry)

#### Limitations:

- Carbon oxidation at hot face (requires protective slag cover or inert atmosphere)
- Higher thermal conductivity increases shell temperature (requires robust safety lining)
- More expensive than MA spinel brick (typically 20–30% higher material cost)

**Best Applications:** High-volume continuous casting operations with controlled slag chemistry and argon

### Alumina-Magnesia Castable (ULCC)

Ultra-low cement castable with  $\text{Al}_2\text{O}_3$  80–90%, MgO 5–10%, designed for monolithic installation. Often in wear resistance.

#### Advantages:

- Rapid installation (no brick laying required)
- Monolithic structure (no mortar joints, eliminates weak points)
- Excellent for complex geometries (bottom impact pads, transitions)
- Lower installed cost (faster turnaround time)

#### Limitations:

- Lower campaign life than brick systems (60–120 heats typical)
- Requires controlled dry-out schedule (moisture-induced spalling risk)
- More sensitive to installation quality (water ratio, mixing, curing)

**Best Applications:** Small to medium ladles, bottom impact pads, repair applications, operations prioritizing

| PROPERTY                          | MA SPINEL BRICK                                   | MGO-C BRICK               |
|-----------------------------------|---------------------------------------------------|---------------------------|
| Composition                       | MgO 60–75%, Al <sub>2</sub> O <sub>3</sub> 15–30% | MgO 75–85%, C 10–18%      |
| Bulk Density (g/cm <sup>3</sup> ) | 2.9–3.1                                           | 2.95–3.15                 |
| CCS (MPa)                         | ≥50                                               | ≥45                       |
| Thermal Conductivity              | Moderate                                          | High (graphite phase)     |
| Slag Resistance                   | Excellent (amphoteric spinel)                     | Outstanding (non-wetting) |
| Thermal Shock Resistance          | Very good                                         | Good                      |
| Campaign Life (heats)             | 80–150                                            | 100–200                   |
| Material Cost (relative)          | 100% (baseline)                                   | 120–130%                  |
| Installation Complexity           | Moderate (brick laying)                           | Moderate (brick laying)   |

## Safety Lining Design and Material Requirements

The safety lining (permanent lining) serves as the critical thermal backup layer, protecting the steel shell during lining campaigns. Standard design specifies high alumina brick (75–85% Al<sub>2</sub>O<sub>3</sub>) with the following performance

- 01 Alumina Content: 75–85% Al<sub>2</sub>O<sub>3</sub> — provides refractoriness under load (RUL) of 1450–1500°C, sufficient for
- 02 Thickness Specification: Small ladles (10–30 ton): 60–75mm; Medium ladles (30–100 ton): 75–90mm; La
- 03 Bulk Density: ≥2.45 g/cm<sup>3</sup> — ensures adequate thermal mass and structural strength

- 04 **Cold Crushing Strength:**  $\geq 55$  MPa — provides mechanical support for working lining and resists compression
- 05 **Thermal Conductivity:** Moderate (0.9–1.2 W/(m·K) at 1000°C) — balances heat dissipation with shell temperature
- 06 **Campaign Life Target:** 3–5 working lining campaigns (equivalent to 300–800 total heats) before requiring replacement

**Common Error:** Using lower-grade fireclay brick ( $\text{Al}_2\text{O}_3$  40–50%) in safety lining to reduce cost. While initial savings occur, the resulting drop in refractoriness leads to premature failure, often requiring complete ladle rebuilds rather than working lining-only replacements.

## Installation Considerations for Safety Lining

Proper safety lining installation is critical for long-term ladle performance:

- **Expansion Gap Design:** Provide 3–5mm expansion joints every 1.5–2.0 meters to accommodate thermal expansion.
- **Anchor System:** Stainless steel or heat-resistant alloy anchors welded to shell, embedded into safety lining.
- **Mortar Selection:** Use high alumina mortar ( $\text{Al}_2\text{O}_3$  matching brick grade  $\pm 5\%$ ) with joint thickness 1–2mm.
- **Dry-Out Schedule:** Controlled heat-up at 20–50°C/hour to 600°C (hold 4–6 hours), then 50–80°C/hour to 1000°C. Avoid rapid heating to prevent induced spalling.

## Bottom Impact Pad Design and Castable Formulation

The bottom impact pad is a critical wear zone absorbing the severe thermal shock and kinetic energy from temperature differential 1200–1500°C in seconds). This zone experiences the highest erosion rate in the working lining campaign.

Impact Pad Material Requirements

Ultra-low cement castable formulations for impact pads must balance:

- **Thermal Shock Resistance:** Monolithic structure (no joints) + low thermal expansion aggregates (and
- **Erosion Resistance:** Hard aggregates (SiC, corundum, tabular alumina) resist abrasive wear from steel
- **Slag Penetration Resistance:** Dense matrix (bulk density  $\geq 2.75 \text{ g/cm}^3$ ) + low CaO content ( $<1.0\%$ )
- **Rapid Strength Development:** Adequate green strength for fast ladle turnaround

| SPECIFICATION                       | STANDARD $\text{Al}_2\text{O}_3$ -MGO ULCC | SIC-ENHANCED ULCC                |
|-------------------------------------|--------------------------------------------|----------------------------------|
| $\text{Al}_2\text{O}_3$ Content (%) | 80–85                                      | 75–80 (+ 8–15% SiC)              |
| MgO Content (%)                     | 8–12                                       | 5–8                              |
| CaO Content (%)                     | $<1.0$                                     | $<0.8$                           |
| Bulk Density ( $\text{g/cm}^3$ )    | 2.75–2.85                                  | 2.70–2.80                        |
| CCS @ 110°C (MPa)                   | $\geq 70$                                  | $\geq 65$                        |
| CCS @ 1000°C (MPa)                  | $\geq 90$                                  | $\geq 85$                        |
| Campaign Life (heats)               | 40–60                                      | 60–80                            |
| Material Cost (relative)            | 100% (baseline)                            | 130–150%                         |
| Best Application                    | General purpose, moderate tapping velocity | High erosion environments, argon |

Installation Parameters for Impact Pad Castable

Critical installation specifications for bottom impact pad castable:

- **Water Addition:** 4.0–5.5% (strictly control to  $\pm 0.3\%$  — excess water reduces density and hot strength

- **Mixing Time:** 4–6 minutes in forced-action mixer (planetary or pan mixer — drum mixers inadequate for
- **Placement Method:** Vibration casting with external form vibration + internal poker (avoid over-vibration)
- **Layer Thickness:** Maximum 150mm per layer — thicker pours risk incomplete consolidation
- **Curing:** Minimum 24 hours at ambient temperature (cover with plastic sheeting to prevent moisture loss)
- **Dry-Out Schedule:**
  - 20°C → 110°C: 10°C/hour (critical moisture release phase)
  - 110°C → 300°C: 15°C/hour (hold 4h at 300°C)
  - 300°C → 600°C: 20°C/hour (dehydration of hydrated phases)
  - 600°C → 1000°C: 50°C/hour (ceramic bond formation)
  - Hold at 1000°C: 4–6 hours (soak for strength development)

**Installation Critical Point:** Rapid dry-out (<15°C/hour below 300°C) is the leading cause of impact pad preheating steam pressure buildup. Always verify ladle heating system can maintain controlled ramp rates — if not, extend preheat to 300°C.

## Campaign Life Optimization Strategies

Maximizing ladle lining campaign life requires attention to material selection, installation quality, and operational practices.

### Working Lining Life Extension Factors

FACTOR 01

**Slag Chemistry Control**

Maintain slag basicity (CaO/SiO<sub>2</sub> ratio) in optimal range for lining material: MA spinel performs best to minimize carbon oxidation. Off-spec slag chemistry reduces campaign life by 30–50%.

FACTOR 02

**Tapping Temperature Management**

Every 20°C increase in tapping temperature above design specification accelerates lining erosion by 10%. Tapping temperature should be minimum required for casting quality, typically 1580–1620°C for continuous casting operations.

FACTOR 03

Argon Stirring Optimization

Excessive argon flow rate (>400 NL/min for 100-ton ladle) creates localized erosion at porous plug and metallurgical objectives — typical range 150–300 NL/min provides adequate mixing with reduced lining wear.

FACTOR 04

Preheating Practice

Inadequate ladle preheating (<1100°C hot face temperature) before steel tapping increases thermal shock stress. Standard practice: preheat to 1200–1300°C hot face temperature, measured with infrared pyrometry.

FACTOR 05

Turnaround Time Control

Rapid thermal cycling (ladle turnaround time <45 minutes) imposes severe thermal shock stress. Allow gradual temperature equilibration — particularly critical for brick working linings.

Field Performance Data: Campaign Life Benchmarks

Industry data from continuous casting operations across China's Zibo steel refractory manufacturing region (integrated steel mills, 2020–2024):

| Ladle Capacity | Working Lining Material                  | Steel Grade     | Average Campaign Life (days) |
|----------------|------------------------------------------|-----------------|------------------------------|
| 30–60 ton      | MA Spinel Brick                          | Carbon steel    | 95–120                       |
| 30–60 ton      | Al <sub>2</sub> O <sub>3</sub> -MgO ULCC | Carbon steel    | 65–85                        |
| 80–120 ton     | MA Spinel Brick                          | Low alloy steel | 80–110                       |
| 80–120 ton     | MgO-C Brick                              | Low alloy steel | 110–150                      |
| 120–200 ton    | MgO-C Brick                              | Stainless steel | 85–120                       |
| All capacities | Impact Pad (SiC ULCC)                    | All grades      | 45–65                        |

*Note: "Best Practice" data represents installations with optimized slag chemistry, controlled tapping temperature, and experienced crews. "Average Campaign" reflects typical field conditions including suboptimal operating parameters.*

### Material Selection Decision Framework

**Choose Magnesia-Alumina Spinel Brick when:** Ladle experiences high slag volumes, frequent thermal cycling. Best balance of performance and cost for most continuous casting operations (target: 80–150 heats).

**Choose Magnesia-Carbon Brick when:** Maximum campaign life is priority, slag chemistry is well-controlled. Best justified by extended service. Best for high-volume operations with consistent metallurgical practices.

**Choose Alumina-Magnesia Castable when:** Fast ladle turnaround is critical, working lining replacement. Ideal for small to medium ladles and repair applications where ladle geometry makes brick installation complex.

### Critical Specifications for Supplier Technical Proposals

When requesting proposals for steel ladle refractory systems, specify the following parameters to enable accurate comparisons:

- 01 Ladle Capacity:** Nominal steel capacity in metric tons (affects lining thickness and material volume)
- 02 Steel Grade:** Carbon steel / Low alloy / Stainless (affects slag chemistry and material selection)
- 03 Tapping Temperature:** Typical range in °C (critical for refractoriness requirements)
- 04 Slag Basicity:** Typical CaO/SiO<sub>2</sub> ratio (determines optimal working lining material family)
- 05 Argon Stirring:** Yes/No, flow rate if applicable (high flow rates require enhanced erosion resistance)
- 06 Turnaround Time:** Typical time between heats in minutes (affects thermal cycling stress)
- 07 Target Campaign Life:** Desired heats per working lining (enables cost-performance optimization)
- 08 Existing Lining Performance:** Current material type and achieved campaign life (benchmark for improvement)

Content developed in collaboration with steel refractory engineering teams from Zibo's specialized ladle l concentration of magnesia-alumina spinel brick, magnesia-carbon brick, and ultra-low cement castable n Asia, Middle East, and Southeast Asia since 1985.

IN THIS ARTICLE

- Ladle Structure & Layers
- Working Lining Materials
- Safety Lining Design
- Bottom Impact Pad
- Campa

FREQUENTLY ASKED QUESTIONS

Steel Ladle Refractory FAQ

- What is the typical campaign life for steel ladle working lining?

+
- Can I use high alumina brick instead of magnesia spinel brick to save cost?

+
- How thick should the safety lining be in a steel ladle?

+
- What is the function of the bottom impact pad in a steel ladle?

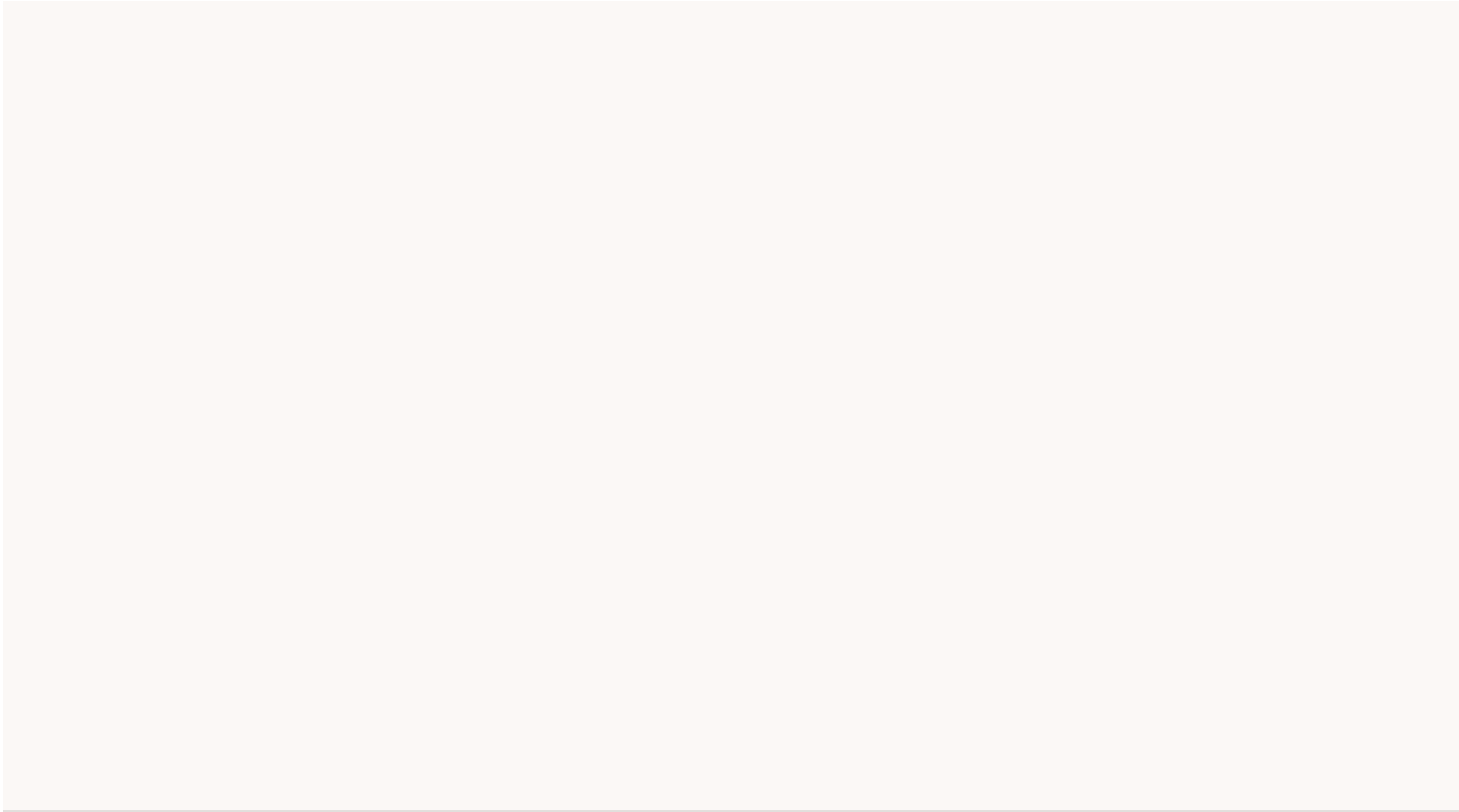
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